

# an exact expression for the thermal variation of the emitter base voltage of bi-polar transistors\*

by R. J. Widlar

Over the years, a number of interesting and useful properties concerning the highly predictable nature of the emitter-base voltage of bi-polar transistors have been discovered. First, it was shown that relationship between the collector current and the emitter-base voltage exactly followed the diode equation over more than eight decades [1], [2]. This has been put directly to use in making logarithmic amplifiers with extremely wide dynamic ranges [3]. Secondly, the theoretically predicted behavior of the emitter-base voltage has made possible dc amplifiers with drifts an order of magnitude lower than can be obtained with conventional techniques [4]. This same theory has been used to produce an ultra-stable, temperature-compensated reference element [5] as well as a low-value current source which does not require large resistance values, making it well suited for integrated circuitry [6], [7]. Lastly, it has been shown that exact temperature compensation of the transconductance can be realized [8]. This has a number of applications including a differential input stage where common mode rejection and gain bandwidth product must be maximized and offset voltage and thermal drift must be minimized, as in a core-memory sense amplifier [9].

This letter will demonstrate another predictable property of the emitter-base voltage in deriving an expression for the emitter-base voltage as a function of temperature in terms of physical constants and the emitter-base voltage at any one temperature. Since a direct attack on this problem quickly produces unwieldy equations, a back-door approach, based on the transconductance-compensation scheme mentioned previously, will be used.

It is shown in [9] that, assuming very high current gains and low-level injection conditions, the voltage gain of the differential amplifier in Fig. 1 will be constant with temperature for

$$V_B = V_{g0} + (n - 1) \frac{kT}{q} \quad (1)$$

Where  $V_{g0}$  is the extrapolated energy gap for the semiconductor material at absolute zero,  $q$  is the charge of an electron,  $n$  is a constant which depends on how the transistor is made,  $k$  is Boltzmann's constant and  $T$  is absolute temperature. The transconductance of the differential pair is

$$\frac{\partial I_c}{\partial V_{BE}} = \frac{qI_c}{2kT} \quad (2)$$

so the gain of the stage is

$$A_v = \frac{qR I_c}{2kT} \quad (3)$$

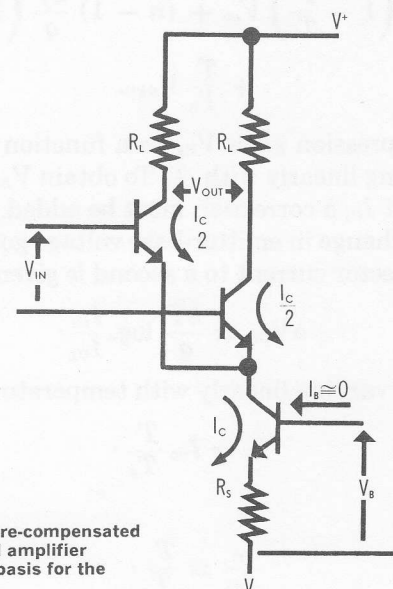


Figure 1  
Temperature-compensated  
differential amplifier  
used as a basis for the  
derivation

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In order to have temperature-stable gain, it must be true that

$$I_C \propto T. \quad (4)$$

From Fig. 1,

$$I_C = \frac{V_B - V_{BE}}{R_S} = BT, \quad (5)$$

where  $B$  is an arbitrary constant. Hence,

$$V_{BE} = V_B - BTR_S. \quad (6)$$

For  $T = T_0$ ,

$$V_{BE0} = V_B - BT_0R_S, \quad (7)$$

and

$$B = \frac{V_B - V_{BE0}}{T_0R_S}. \quad (8)$$

Substitution into equation (6), this becomes

$$V_{BE} = \left(1 - \frac{T}{T_0}\right)V_B + \frac{T}{T_0}V_{BE0}. \quad (9)$$

Using equation (1) for  $V_B$ ,

$$V_{BE} = \left(1 - \frac{T}{T_0}\right)V_{g0} + (n-1)\frac{kT}{q}\left(1 - \frac{T}{T_0}\right) + \frac{T}{T_0}V_{BE0}. \quad (10)$$

This expression gives  $V_{BE}$  as a function of  $T$  for  $I_C$  varying linearly with  $T$ . To obtain  $V_{BE}(T)$  for constant  $I_C$ , a correction must be added.

The change in emitter-base voltage going from one collector current to a second is given by

$$\Delta V_{BE} = \frac{kT}{q} \log_e \frac{I_{C2}}{I_{C1}}. \quad (11)$$

With  $I_C$  varying linearly with temperature,

$$I_C = I_{C0} \frac{T}{T_0}. \quad (12)$$

Hence,

$$\frac{I_C}{I_{C0}} = \frac{T}{T_0}, \quad (13)$$

and

$$\Delta V_{BE} = \frac{kT}{q} \log_e \frac{T_0}{T}. \quad (14)$$

This is the change in emitter base voltage caused by maintaining a constant collector current. The complete expression for  $V_{BE}(T)$  is then

$$V_{BE} = \left(1 - \frac{T}{T_0}\right)V_{g0} + V_{BE0} \frac{T}{T_0} + \frac{kT}{q} \log_e \frac{T_0}{T} + (n-1)\frac{kT}{q}\left(1 - \frac{T}{T_0}\right) \quad (15)$$

The extrapolated energy gap ( $V_{g0}$ ) for silicon is 1.205 V,  $k/q$  has a value of  $8.66 \times 10^{-5}$  V/°C and the constant  $n$ , has a typical value of 1.5 for double-diffused silicon transistors.

To give some appreciation for the magnitude of the terms in (15) a sample calculation can be made for  $T_0 = 25^\circ\text{C}$ .  $V_{BE0} = 670$  mV and  $T = 125^\circ\text{C}$ :

$$V_{BE} = -0.403 + 0.894 - 0.010 - 0.006 = 0.476 \text{ V}.$$

This shows that the last two terms of (15) are relatively small, making  $V_{BE}$  nearly a linear function of  $T$  as is popularly assumed.

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